

AN UNCERTAINTY MODEL OF A NON-IDEAL OPEN AREA TEST SITE
FOR ELECTROMAGNETIC MEASUREMENT

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to my beloved wife Ester, my son Marvel, and my daughter Ceara



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ABSTRACT

An open area test site (OATS) is a standard facility to perform electromagnetic compatibility (EMC) compliance testing of electrical and electronic products. An ideal OATS is a flat area, free of any obstructions and external signals. Pre-compliance testing in a non-ideal OATS is an economical way to prepare a product for compliance testing. However, measurements in the non-ideal OATS have higher uncertainty. In addition, the existing model to analyse the measurement uncertainty is not adequate. Therefore, this research proposes an uncertainty model of a non-ideal OATS for electromagnetic measurement to analyse the measurement uncertainty components in the non-ideal OATS. In this research a normalized site attenuation (NSA) measurement uncertainty model was derived. A 3-m non-ideal OATS has been designed and built. The suitability of the location to build the OATS has been evaluated. To evaluate the measurement uncertainty in the site and the closeness of the site NSA to the ideal NSA, a series of NSA measurements in the non-ideal OATS were performed in the frequency range of 300 MHz to 1000 MHz. From the analysis, the expanded uncertainties of the OATS with a coverage factor of 2 were in the range of ± 1.68 dB to ± 1.98 dB. Besides, the OATS NSA values were inside ± 4 dB margins as specified in CISPR 16-1-4:2010 standard. Therefore, the non-ideal OATS is eligible for pre-compliance testing. Based on many factors investigated in the sensitivity analysis, it was found that the dominant factor that contributed to the measurement uncertainty in the non-ideal OATS came from the antennas. In summary, this research mainly contributes to the development and evaluation of a low cost non-ideal OATS for pre-compliance testing.

ABSTRAK

Tapak uji kawasan terbuka (OATS) adalah kemudahan piawai untuk melaksanakan ujian kepatuhan keserasian elektromagnet (EMC) untuk produk elektrik dan elektronik. OATS yang unggul adalah kawasan yang rata, bebas daripada apa-apa halangan dan isyarat luar. Ujian pra-pematuhan dalam OATS tidak unggul semasa pembangunan produk adalah cara yang ekonomi untuk menyediakan produk untuk ujian kepatuhan. Walau bagaimanapun, pengukuran dalam OATS tidak unggul mempunyai ketidaktentuan lebih tinggi. Di samping itu, model yang ada untuk menganalisis ketidaktentuan pengukuran itu tidak mencukupi. Oleh itu, kajian ini mencadangkan model ketidaktentuan OATS tidak unggul untuk pengukuran elektromagnet digunakan untuk menganalisis komponen ketidaktentuan pengukuran dalam OATS tidak unggul. Dalam kajian ini, model ketidaktentuan pengukuran pelemahan tapak ternormal (NSA) diterbitkan. OATS tidak unggul 3-m telah direka dan dibina. Kesesuaian lokasi untuk membina OATS telah dinilai. Untuk menilai ketidakpastian pengukuran di tapak dan kedekatan NSA tapak kepada NSA unggul, satu siri pengukuran NSA dalam OATS tidak unggul telah dilakukan dalam julat frekuensi 300 MHz hingga 1000 MHz. Dari analisis, ketidakpastian OATS terkembang dengan faktor liputan 2 berada dalam julat ± 1.68 dB hingga ± 1.98 dB. Selain itu, nilai NSA OATS berada dalam jidar ± 4 dB seperti dinyatakan dalam piawaian CISPR 16-1-4:2010. Oleh itu, OATS tidak unggul layak untuk ujian pra-kepatuhan. Berdasarkan banyak faktor yang disiasat dalam analisis kepekaan, didapati bahawa faktor dominan yang menyumbang kepada ketidakpastian pengukuran dalam OATS tidak unggul datang dari antena. Ringkasnya, penyelidikan ini menyumbang kepada pembangunan dan penilaian OATS tidak unggul dengan kos rendah untuk ujian pra-kepatuhan.

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LIST OF SYMBOLS AND ABBREVIATIONS

SYMBOLS

A	-	antenna aperture
A_N	-	normalized site attenuation
AF_r	-	receive antenna factor
AF_t	-	transmit antenna factor
b	-	surface height variation
c	-	velocity of light
c_i	-	sensitivity coefficients
d	-	deviation
d	-	distance
d_d	-	direct path from transmit to receive antenna
d_r	-	reflected path from transmit to receive antenna
E	-	electric field intensity
\mathbf{E}	-	electric field intensity vector
\mathbf{E}_d	-	direct electric field intensity vector
\hat{E}_h	-	normalized electric field intensity for horizontal polarization
E_{\max}	-	maximum electric field in receive-antenna height-scanned between $h_{r\min}$ to $h_{r\max}$
\mathbf{E}_m	-	reflected electric field intensity vector
\hat{E}_v	-	normalized electric field intensity for vertical polarization
f	-	function
f_M	-	frequency = $300/\lambda$ MHz
F_r	-	receive antenna directivity

F_t	-	transmit antenna directivity
$F_r(\theta)$	-	normalized radiation pattern of receive antenna in vertical plane
$F_r(\varphi)$	-	normalized radiation pattern of receive antenna in horizontal plane
$F_t(\theta)$	-	normalized radiation pattern of transmit antenna in vertical plane
$F_t(\varphi)$	-	normalized radiation pattern of transmit antenna in horizontal plane
g_r	-	receive antenna gain
g_t	-	transmit antenna gain
h_r	-	receive antenna height
h_t	-	transmit antenna height
H	-	magnetic field intensity
\mathbf{H}	-	magnetic field intensity vector
I_0	-	peak value of current of a dipole
I_t	-	transmit antenna current
k	-	coverage factor
k	-	number of different series of measurement
l	-	length
L	-	length of a dipole
n	-	number of observations
p	-	probability density
\mathbf{P}	-	power density vector
P_d	-	power density
P_r	-	power delivered to load
P_t	-	power transmitted
\bar{q}	-	arithmetic mean of observation
q_k	-	individual observations
r	-	horizontal distance between transmit and receive antenna
R_{dr}	-	detector resistance
R_{lr}	-	receive antenna loss resistance
R_{lt}	-	transmit antenna loss resistance

R_{rr}	-	receive antenna reradiating resistance
R_{rt}	-	transmit antenna radiation resistance
R_{sg}	-	signal generator resistance
s	-	standard deviation
s_p	-	pooled experimental standard deviation
u	-	uncertainty
u_c	-	standard uncertainty
U	-	expanded uncertainty
V_{dir}	-	direct voltage
V_{oc}	-	open circuit voltage induced by incident electrical field across receive antenna
V_{sg}	-	signal generator voltage
V_{site}	-	site voltage
V_r	-	load voltage
V_t	-	transmit antenna voltage
X_{dr}	-	detector reactance
X_r	-	receive antenna reactance
X_{sg}	-	signal generator reactance
X_t	-	transmit antenna reactance
Z_0	-	impedance of space = $120\pi \Omega$
Z_{in}	-	input impedance
Z_{sg}	-	signal generator impedance
Z_t	-	transmit antenna impedance
Z_L	-	load impedance
Z_s	-	source impedance
β	-	free space wavenumber
δAF_r	-	correction for receive antenna factor
δAF_t	-	correction for transmit antenna factor

δb	-	correction for ground plane roughness
δf_M	-	correction for signal generator frequency
δp_c	-	correction for antenna phase centre location
δr	-	correction for antennas separation distance
δh_t	-	correction for imperfect transmit antenna height
δR_{dir}	-	correction for measurement repeatability of direct voltage
δR_{site}	-	correction for measurement repeatability of site voltage
δV_{sadir}	-	correction for spectrum analyser voltage reading when directly connected to signal generator
δV_{sgdir}	-	correction for signal generator voltage reading when directly connected to spectrum analyser
δV_{sasite}	-	correction for spectrum analyser voltage reading when performing site voltage measurement
δV_{sgsite}	-	correction for signal generator voltage reading when performing site voltage measurement
ϵ_0	-	permittivity of vacuum = 8.85419×10^{-12} F/m
ϵ_{r2}	-	relative dielectric constant
Φ	-	phase shift due to the reflection
γ	-	grazing angle
Γ	-	ground plane reflection coefficient
Γ_h	-	horizontal reflection coefficient
Γ_v	-	vertical reflection coefficient
η_0	-	intrinsic impedance of free-space
λ	-	wavelength
μ_0	-	permeability of vacuum = $4\pi \times 10^{-7}$ H/m
θ_d	-	incident angle of direct path
θ_r	-	incident angle of reflected path
σ	-	variance
σ_2	-	ground plane conductivity

ω - radian frequency

ABBREVIATIONS

<i>AC</i>	-	Alternating Current
<i>AF</i>	-	Antenna Factor
<i>ANSI</i>	-	American National Standard Institute
<i>CALTS</i>	-	Calibration Test Site
<i>CDMA</i>	-	Code Division Multiple Access
<i>CENELEC</i>	-	Comité Européen de Normalisation Electrotechnique
<i>CISPR</i>	-	Comité International Spécial des Perturbations Radioélectriques
<i>COMTS</i>	-	Compliant Test Site
<i>EMC</i>	-	Electromagnetic Compatibility
<i>EMI</i>	-	Electromagnetic Interference
<i>ESDM</i>	-	Experimental Standard Deviation of the Mean
<i>EU</i>	-	European Union
<i>EUT</i>	-	Equipment Under Test
<i>FCC</i>	-	Federal Communications Commission
<i>FDTD</i>	-	Finite Difference Time Domain
<i>FM</i>	-	Frequency Modulation
<i>FSAF</i>	-	Free Space Antenna Factor
<i>GSM</i>	-	Global System for Mobile Communications
<i>GSAF</i>	-	Geometry-Specific Antenna Factor
<i>GUM</i>	-	Guide to the Expression of Uncertainty in Measurement
<i>ISO</i>	-	International Standards Organization
<i>IEC</i>	-	International Electrotechnical Commission
<i>JGCM</i>	-	Joint Committee for Guides in Metrology
<i>LPDA</i>	-	Log Periodic Dipole Antenna
<i>MS</i>	-	Malaysian Standards
<i>NSA</i>	-	Normalized Site Attenuation
<i>OATS</i>	-	Open Area Test Site
<i>PC</i>	-	Phase Center
<i>RF</i>	-	Radio Frequency

<i>SA</i>	-	Site Attenuation
<i>SAC</i>	-	Semi Anechoic Chamber
<i>SGP</i>	-	Smith, German, & Pate
<i>SSE</i>	-	Sum of Squares due to Error
<i>SSM</i>	-	Standard Site Method
<i>TAM</i>	-	Three Antenna Method
<i>TV</i>	-	Television
<i>TNSA</i>	-	Theoretical Normalized Site Attenuation
<i>UHF</i>	-	Ultra High Frequency
<i>US</i>	-	United States
<i>UTHM</i>	-	Universiti Tun Hussein Onn Malaysia
<i>VHF</i>	-	Very High Frequency
<i>VIM</i>	-	International Vocabulary of Basic and General Terms in Metrology



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CHAPTER 1

INTRODUCTION

1.1 Background

According to the International Electrotechnical Vocabulary by the International Electrotechnical Commission, electromagnetic compatibility (EMC) is defined as “the ability of an equipment or system to function satisfactorily in its electromagnetic environment without introducing intolerable electromagnetic disturbances to anything in that environment” (International Electrotechnical Commission, 2017, para. 1). In order to function satisfactorily, the equipment or system has to also possess good immunity or susceptibility from electromagnetic interference (EMI). For example, it is necessary for a pacemaker not to produce any electromagnetic disturbance to the environment but more importantly, it has to be immune from self-interference as well as any outside EMI. In short, an electromagnetically compatible system does not interfere with the operations of other systems as well as its own operation and is immune from the emissions of other systems (Goedbloed, 1992). Hence, the field of EMC covers the electromagnetic emission issues which refer to the unwanted generation of electromagnetic energy by the equipment and the electromagnetic immunity or susceptibility issues which are related to the correct operation of the equipment in the presence of unwanted EMI.

Testing and evaluation for EMC involve the measurements of radiated emission, conducted emission, radiated susceptibility and conducted susceptibility (Montrose & Nakauchi, 2004). The radiated emission testing is done to measure EMI generated by equipment under test (EUT) which is radiated through the space (Agilent Technologies, 2010). The conducted emissions testing measures the unwanted signals that are on the AC power mains generated by EUT (Agilent

Technologies, 2010). The radiated susceptibility testing is conducted to determine the EUT's ability to operate in the presence of EMI propagated via space (Aero Nav Laboratories, 2014). The conducted susceptibility testing is performed to determine the EUT's ability to operate in the presence of EMI propagated via a conductor (Aero Nav Laboratories, 2014).

Among the above mentioned types of EMC testing, the radiated emission testing is mandated to be measured in an open area test site (OATS) as described in CISPR 11 (2010a), CISPR 22 (2008), CISPR 16-1-4 (2010b) and ANSI C63.7 (2015). The radiated emission testing measures the electromagnetic emissions emanating from EUT. The purpose of the testing is to verify the EUT's ability to remain below specified electromagnetic emissions levels during its operation.

EMC testing is now a requirement of many global conformance and safety standards to many sectors including telecommunication, automotive, medical and consumer electronics. Many countries around the world have seen the importance of EMC. Therefore, EMC has become an important part of product design. In addition, compliance to EMC standards is required for importing electrical and electronic products into many countries world-wide (Armstrong & Williams, 2001). For instance, in Europe, the European Committee for Electrotechnical Standardization (CENELEC) on 1 January 1996 issued a mandatory directive regarding products to be marketed in the European Union (EU). This directive made it mandatory for electrical and electronic equipment which is to be sold in Europe meet certain requirements regarding electromagnetic emission and immunity (Singh & Garg, 1999).

EMC compliance testing is an activity to assess the compliance of a product to an EMC regulation or standard before the product may be exported. In order to get the certificate of compliance, the testing must be performed in a certified laboratory. The standard in the EMC compliance testing depends on which country the product will be sold. For example, information technology equipment to be sold in the US must be tested to comply FCC part 15 regulations, whereas if the product will be sold to Europe, it must be comply to EN55022 (CISPR 22) (Agilent Technologies, 2010).

Considering that the EMC compliance testing is relatively expensive and there is no guarantee that a product will pass the testing in one shot, it will be effective if preliminary testing which is usually called EMC pre-compliance testing

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