

OPTIMISATION DEEP DRAWING PROCESS PARAMETERS USING FE
SIMULATION

MOHD NIZAM BIN KATIMON

A project report submitted in partial
fulfillment of the requirement for the award of the
Degree of Master of Mechanical Engineering

Faculty of Mechanical and Manufacturing Engineering
Universiti Tun Hussein Onn Malaysia

MARCH, 2008

Untuk tersayang isteriku Rosnah bt Mohd Zin yang sentiasa memberikan dorongan dan semangat, Nurul Husna yang kadangkala 'membantu', Ayahanda Katimon b Samin serta Ibunda Siti Ahasah bt Hj A. Kadir yang sentiasa mendoakan kejayaan ini dan tidak dilupakan sahabat karib yang banyak membantu diatas kejayaanku ini.



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH

ACKNOWLEDGEMENT

IN THE NAME OF ALLAH, THE MOST GRACIOUS, THE MOST MERCIFUL.

I would like to take this opportunity to acknowledge Dr. Ing Haryanti Samekto as my supervisor and Assoc. Prof. Mustafa Yusof from UTM, Skudai for guide and helping me in carrying out this project.

To all of those that I could not mention by name, I appreciate everything you all have done for me. May God bless you and hope you guys to continue these good altitudes.



PT TAAUTAHIM
PERPUSTAKAAN TUNKU TUN AMINAH

ABSTRACT

This paper presents the modeling simulation and experimental validation of cylindrical cup deep drawing. Prediction of the deep drawing results which includes determination of the optimum Blank Holder Force (BHF) and the thickness distribution of the sheet metal (blank) will decrease the production cost and time. Before performing the Finite Element (FE) analysis, it is required to understand the sheet metal (blank) properties and material model. In this FE analysis, the effect of fixed BHF on the cylindrical cup wall thickness distribution is examined. According to the experimental study, the optimum and maximum values of fixed BHF was at 1 kN and 11 kN respectively. These values are determined without the blank exceeding the tearing limits. Comparison of simulation and experimental study indicates that the FE model is considered valid, which can be seen from the similar thickness profile of simulation and experimental results.



PT. AMINAH
PERPUSTAKAAN

ABSTRAK

Kajian tesis ini berkaitan simulasi permodelan dan pengesahan eksperimen terhadap cawan silinder penarikan dalam. Jangkaan keputusan penarikan dalam yang mencakupi penentuan nilai optimum daya pemegang contoh-kosong (*BHF*) dan agihan ketebalan kepingan logam (*blank*) akan mengurangkan kos dan masa proses pengeluaran. Sebelum melakukan analisa Unsur Terhingga, ia memerlukan pemahaman berkaitan sifat-sifat kepingan logam dan pemodelan bahan. Di dalam analisa Unsur Terhingga, kesan daya tetap *BHF* terhadap agihan ketebalan dinding cawan silinder dikaji. Melalui kajian eksperimen, nilai optimum dan maksimum *BHF* ialah 1 kN dan 11 kN masing-masing. Nilai ini ditentukan tanpa *blank* melebihi tahap kegagalan koyak. Perbandingan di antara kajian simulasi dan eksperimen menunjukkan model Unsur Terhingga boleh digunakan, ia diperhatikan daripada keputusan bentuk ketebalan di antara simulasi dan eksperimen yang menunjukkan kesamaan.



PERPUSTAKAAN UNIVERSITI AMINAH

TABLE OF CONTENTS

CHAPTER	TITLE	PAGE
	ACKNOWLEDGEMENT	iv
	ABSTRACT	v
	ABSTRAK	vi
	TABLE OF CONTENTS	vii
	LIST OF TABLES	x
	LIST OF FIGURES	xiii
	LIST OF SYMBOLS	xvii
	LIST OF ABBREVIATION	xix
	LIST OF APPENDIXES	xx
I	INTRODUCTION	
	1.1 Introduction	1
	1.2 Problem Statement	3
	1.3 Objectives	4
	1.4 Scope	4
	1.5 Research Methodology	5
II	LITERATURE REVIEW	
	2.1 Introduction	7
	2.2 Aluminum	8
	2.3 Deep drawing	9
	2.3.1 Plastic Deformation	10

2.3.2	Deep Drawing Parameters	14
2.3.3	Anisotropy	20
2.3.4	Height of Cylindrical Cups	22
2.4	FE Simulation	23
2.4.1	Material Model	23
2.4.2	Principles of FEM	25
2.4.3	Classification of Finite-Element Formulation	27
2.4.4	Recent Researches on Deep Drawing Simulation	28

III

EXPERIMENTAL STUDY

3.1	Tensile Test	31
3.1.1	Specimen Preparations	32
3.1.2	Tensile Test Parameters	33
3.1.3	Tensile Result	34
	3.1.3.1 Engineering Stress-Strain Curve	35
	3.1.3.2 True Stress-Strain Curve	36
	3.1.3.3 Logarithmic Diagram	37
3.2	Material Model	39
3.3	Erichsen Cupping Test	44
	3.3.1 Blank Holder Force	46
	3.3.2 Result on Thickness Distribution	48
	3.3.3 Heights of Cups	49
3.4	Anisotropy	51
3.5	Deep Drawing Defects	52

IV

FINITE ELEMENT SIMULATION

4.1	Introduction	54
4.2	About ABAQUS	55
4.3	Creating the Model	56

4.4	Tools Definition	58
4.5	Blank Definition	58
4.5.1	Material Properties	58
4.5.2	Element	60
4.6	Contact Interactions	60
4.7	Process Modeling Idealization	61
4.8	Boundary Conditions	62
4.9	Result on Thickness Distribution	63
4.10	Results on Plastic Strain	65
4.11	Predicted Thickness at Different Punch Displacement	71

V

ANALYSIS AND DISCUSSIONS

5.1	Experimental Study Result	75
5.1.1	Determine the Optimum BHF	75
5.1.2	The Effect of BHF on Thickness Distribution	76
5.1.3	Deep Drawing Force	77
5.1.4	The Effects of Constant BHF on Deep Drawing Effects	78
5.2	Simulation Results	80
5.2.1	Flow of Material	80
5.3	Comparison the Thickness Distribution between Experimental and Simulation	81

VI

CONCLUSIONS	93
--------------------	----

REFERENCES	94
-------------------	----

LIST OF TABLES

TABLE NO.	TITLE	PAGE
2.1	Cylindrical cup test: process parameters	18
2.2	Process parameters	19
3.1	Tensile test specimen dimension	33
3.2	Maximum load and maximum displacement at different rolling direction	34
3.3	Materials properties of Al 5182	39
3.4	The mean difference for yield strength between material model and experimental for 0 ⁰ rolling direction	41
3.5	The mean difference for yield strength between material model and experimental for 45 ⁰ rolling direction	42
3.6	The mean difference for yield strength between material model and experimental for 90 ⁰ rolling direction	43
3.7	Process parameters for cylindrical cup test	46
3.8	Thickness distribution for experimental at different position respective to BHF	48
3.9	The height of cylindrical cup at different BHF	50
3.10	The height of the cup between experimental and mathematical	50

3.11	Experimental result for r-value for 90° to the rolling direction	51
3.12	Experimental result for r-value for 45° to the rolling direction	51
3.13	Experimental result for r-value for 0° to the rolling direction	52
4.1	Yield stress- plastic strain data	59
4.2	Summary of boundary conditions applied in Step 1	63
4.3	Thickness distribution for simulation at different point respective to BHF	64
4.4	Thickness distribution at different punch displacement for 1 kN BHF	71
5.1	Cylindrical cup: Thickness at different position for experimental and simulation at 1 kN BHF	82
5.2	Cylindrical cup: Thickness at different points for experimental and simulation at 2 kN BHF	83
5.3	Cylindrical cup: Thickness at different points for experimental and simulation at 3 kN BHF	84
5.4	Cylindrical cup: Thickness at different points for experimental and simulation at 4 kN BHF	85
5.5	Cylindrical cup: Thickness at different points for experimental and simulation at 5 kN BHF	86
5.6	Cylindrical cup: Thickness at different points for experimental and simulation at 6 kN BHF	87
5.7	Cylindrical cup: Thickness at different points for experimental and simulation at 7 kN BHF	88
5.8	Cylindrical cup: Thickness at different points for experimental and simulation at 8 kN BHF	89
5.9	Cylindrical cup: Thickness at different points for experimental and simulation at 9 kN BHF	90

5.10	Cylindrical cup: Thickness at different points for experimental and simulation at 10 kN BHF	91
5.11	Cylindrical cup: Thickness at different points for experimental and simulation at 11 kN BHF	92



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH

LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	The flow chart of the project	6
2.1	Load-Displacement diagram for 0° rolling direction	10
2.2	Engineering stress-strain curve for 0° rolling direction	11
2.3	Log sigma-Log epsilon for Plastic area	13
2.4	Schematic diagram of deep drawing cylindrical cup	15
2.5	The definition of BHF formability window by Lin Z. Q., Wang W. R. and Chen G. L. (2007)	16
2.6	BHF at tearing and wrinkling for various strains hardening exponent by Choudhury I. A., Lai O. H. and Wong L. T. (2005)	17
2.7	Cylindrical cup test: problem layout	18
2.8	Effect of normal anisotropy on the limiting drawing ratio by K. Lange <i>et al.</i> (1985)	22
3.1	Tensile Test Specimen	32
3.2	Diagram of rolling direction	32
3.3	Graph Force-Displacement for specimen at different rolling direction	34
3.4	Stress-strain diagram for engineering data	36
3.5	Stress-strain diagram for true data	37

3.6	True stress-strain at plastic area in logarithmic diagram	38
3.7	Graph comparison between material model with experimental for 0° rolling direction	40
3.8	Graph comparison between material model with experimental for 45° rolling direction	42
3.9	Graph comparison between material model with experimental for 90° rolling direction	43
3.10	Illustration after Erichsen test	45
3.11	Tooling system for deep drawing experiment	45
3.12	Graph drawing force-drawing stroke	47
3.13	The experimental results of Erichsen test	47
3.14	Cross-sectional view for the location of position (mm)	48
3.15	Thickness distribution for experimental	49
3.16	Specimen diagram to determined r-value	51
3.17	Earring start occurred at 3 kN BHF	52
3.18	Earring occurred on both sides at 11 kN BHF	53
3.19	Tears start occurred at 12 kN BHF	53
4.1	Cylindrical deep drawing analysis	57
4.2	Dimensions (mm) of the components in the forming simulation	57
4.3	Yield stress-plastic strain	59
4.4	Mesh for the blank in the simulation	60
4.5	Illustration of contact interactions for forming simulation	61
4.6	Thickness distribution for simulation	64
4.7	Thickness distribution for simulation at 1 kN BHF	65
4.8	Thickness distribution for simulation at 2 kN BHF	65

4.9	Thickness distribution for simulation at 3 kN BHF	66
4.10	Thickness distribution for simulation at 4 kN BHF	66
4.11	Thickness distribution for simulation at 5 kN BHF	67
4.12	Thickness distribution for simulation at 6 kN BHF	67
4.13	Thickness distribution for simulation at 7 kN BHF	68
4.14	Thickness distribution for simulation at 8 kN BHF	68
4.15	Thickness distribution for simulation at 9 kN BHF	69
4.16	Thickness distribution for simulation at 10 kN BHF	69
4.17	Thickness distribution for simulation at 11 kN BHF	70
4.18	Thickness distribution for simulation at 12 kN BHF	70
4.19	Simulation thickness distribution at 1 kN BHF	72
4.20	Simulation at 5 mm punch displacement for 1 kN BHF	72
4.21	Simulation at 10 mm punch displacement for 1 kN BHF	73
4.22	Simulation at 15 mm punch displacement for 1 kN BHF	73
4.23	Simulation at 20 mm punch displacement for 1 kN BHF	74
4.24	Simulation at 23 mm punch displacement for 1 kN BHF	74
5.1	Experimental result at different BHF	76

5.2	Thickness distribution for experimental at different BHF	77
5.3	Graph Drawing Force-Drawing Stroke at different BHF	78
5.4	Earring did not occur at 1 kN and 2 kN BHF	79
5.5	Earring start occurred at two sides of cup at 5 kN BHF	79
5.6	Earring occurred at two sides of cup at 11 kN BHF	80
5.7	Thickness profile at 1 kN BHF between experimental and simulation	82
5.8	Thickness profile at 2 kN BHF between experimental and simulation	83
5.9	Thickness profile at 3 kN BHF between experimental and simulation	84
5.10	Thickness profile at 4 kN BHF between experimental and simulation	85
5.11	Thickness profile at 5 kN BHF between experimental and simulation	86
5.12	Thickness profile at 6 kN BHF between experimental and simulation	87
5.13	Thickness profile at 7 kN BHF between experimental and simulation	88
5.14	Thickness profile at 8 kN BHF between experimental and simulation	89
5.15	Thickness profile at 9 kN BHF between experimental and simulation	90
5.16	Thickness profile at 10 kN BHF between experimental and simulation	91
5.17	Thickness profile at 11 kN BHF between experimental and simulation	92



LIST OF SYMBOLS

S_u	-	ultimate tensile strength
S_0	-	initial sheet thickness
r	-	normal anisotropy
\bar{r}	-	average normal anisotropy
c	-	constant value lies between 2 and 3
h_c	-	height of the cup
d_0	-	initial diameter of
v^T	-	nodal point velocities
Δr	-	planar anisotropy
A	-	current section area
A_0	-	initial cross sectional area
F	-	load on the specimen
f	-	the residual of the nodal point force vector.
\mathbf{K}	-	stiffness matrix
K	-	strength coefficient
L	-	current length
L_0	-	initial length
ΔL	-	displacement

Greek symbols

β	-	drawing ratio
μ	-	coefficient of friction
ε_{true}	-	true strain
σ_{true}	-	true stress
v	-	punch speed
ε_0	-	initial strain
ε^P	-	plastic strain

Superscripts

n	-	strain hardening coefficient
T	-	transposition



LIST OF ABBREVIATION

BHF	-	Blank Holder Force
FE	-	Finite Element
FLD	-	Forming Limit Diagram
LDR	-	Limiting Drawing Ratio
PBH	-	Blank Holder Pressure



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH

LIST OF APPENDIXES

APPENDIX	TITLE	PAGE
A	Material Properties AL 5182	97
B	Input Files for ABAQUS Simulation	98
C	Graph for Tensile Test	106



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH

CHAPTER I

INTRODUCTION

1.1 Introduction

The main strategy of automotive industry to reduce fuel consumption is to increase the percentage of light materials in car, mainly outer body. The main reason of this direction is because by reducing the weight of the car means increasing mileage per liter of fuel. The benefits of this are not only to reduce fuel consumption but also to protect our environment. The need to improve fuel economy and reduce emissions is an opportunity to expand the applications of light materials, particularly in body structures.

Energy use and the CO₂ emissions caused by transport have increased significantly. This increase has been caused by the rapid growth in the size of the world's vehicle fleet. The manufacturers of vehicles and their suppliers are seeking ways to reduce the environmental impacts caused by transport. Different life cycle assessments have shown that reducing 1kg of a car body saves about 20 kg of greenhouse gas emissions (in CO₂ equivalents).

Aluminum alloy can be categorized as a relatively light metal compared to metals such as steel, nickel, brass, and copper with a specific gravity of 2.7. It is a silverish white metal that has a strong resistance to corrosion which is a result of an oxide skin formed as a result of reactions with the atmosphere. This corrosive skin protects aluminum from most chemicals, weathering conditions, and even many acids. However alkaline substances are known to be able to penetrate the protective skin and corrode the metal.

Aluminum alloy is easy to machine and can have a wide variety of surface finishes. It is a very versatile metal and can be casted in any form. It can be rolled, stamped, drawn, spun, roll-formed, hammered and forged. The metal can be extruded into a variety of shapes, and can be turned, milled, and bored in the machining process. Aluminum can be riveted, welded, brazed, or resin bonded. For most applications, aluminum needs no protective coating as it can be finished to look good, however it is often anodized to improve color and strength

Deep drawing is one of the most important processes for sheet metal forming which is also widely used to fabricate automotive components such as Panel Floor Reinforcement and Support Grille Assembly. Deep drawing is a process in which a blank or work piece usually controlled by a pressure plate is forced into and/ or through a die by means of a punch to form a hollow component. The thickness is substantially the same as that of the original material. It is a complex forming process which is governed by many different parameters.

FE simulation is a method which can be applied to determine the optimum process parameters in deep drawing. It is a computer simulation technique used in engineering analysis. It uses a numerical technique called finite element method. The basic concept of the finite element method is discretization. A number of finite points are identified in the domain of the function. The values of the function and its derivatives when appropriate are specified at these points. The points are called

nodal points. The domain of the function is represented approximately by a finite collection of subdomains called finite elements.

The main advantages of the finite-element method are the capability of obtaining detailed solutions of the mechanics in a deforming body, namely velocities, shapes, strains, stresses, temperatures or contact pressure distributions.

1.2 Problem Statement

Aluminum alloy or AA 5182 is a wrought aluminum in 5000 series. This AA 5182 has a limiting formability, therefore, it is important to determine the material limitation. Blank holder force (BHF) is one of the important parameters to control the wrinkle and tears of product. Each material with geometry product should have BHF limits where lower BHF cause the possible of wrinkle while higher BHF cause the possible of tears.

Finite element method (FEM) is a very effective method to simulate the forming processes with accurate prediction of the deformation behaviors. FEM can be used not only in the analysis but also in the design to estimate the optimum conditions of the forming processes. This can be done before carrying out the actual experiments for an economical and successful application to industrial components.

Trial and error is a common method that used in industry to determine blank holder force (BHF) which is takes a lot of time and very costly. Numerical simulation is a method to get fast result and inexpensive to determine optimum BHF. However, to perform numerical simulation the followings must be comprehended:

- a. Material properties of the blank (Aluminum sheet metal).
- b. Representative material constitutive equation.
- c. Understanding the interaction between part geometry during process.

1.3 Objectives

The main objectives of this work are:

1. Determine the material properties of aluminum alloy 5182 in order to obtain valid input of material parameters in material model.
2. Select the material model for aluminum alloy 5182.
3. Conduct FE simulation using FE software with applicable non-linear transient dynamic analysis to determine optimum BHF value respect to friction coefficient (μ) and punch speed (v).

1.4 Scope

1. Material: Aluminum 5182.
2. Geometry Product: Cylindrical Cup.
3. Modeling and Simulation: Using FE software (ABAQUS CAE) to perform finite element analysis.
4. Experimental: Using Erichsen Test Machine and Universal Tensile Test.
5. Parameters: Fix the friction coefficient (μ) and punch speed (v).

1.5 Research Methodology

The details of the methodologies are explained in Chapter III and IV. Below are the summary of this research methodology.

1. Material Testing
Perform tensile test on Aluminum 5182 sheet metal according to ASTM E8.
2. Material Model
Select the modeling material behavior in deep drawing process for Aluminum 5182.
3. FE simulation
Using FE software (ABAQUS CAE) to simulate optimum blank holder force (BHF) which respect to friction coefficient (μ) and punch speed (v).
4. Experimental
Using selected BHF to determine percent of error between simulation and experimental result based on the thickness distribution.



PTIA UTHM
PERPUSTAKAAN TUN AMINAH

REFERENCES

- A. G. Mamalis, D.E. Manolacos and A.K. Baldoukas (1997). "Simulation of sheet metal forming using explicit finite-element techniques: effect of material and forming characteristics. Part I. Deep-drawing of cylindrical cups." *Journal of Materials Processing Technology* 72. 48–60.
- C. Garcia *et al.* (2006). "Numerical modeling and experimental validation of steel deep drawing processes. Part II: Applications." *Journal of Materials Processing Technology* 172. 461–471.
- Choudhury I. A., Lai O.H. and Wong L.T (2006). "PAM-STAMP in the simulation of stamping process of an automotive component." *Simulation Modeling Practice and Theory* 14. 71-81.
- Demirci, H. I. *et al.* (2008). "The theoretical and experimental investigation of blank holder forces plate effect in deep drawing process of AL 1050 material." *Journals of Materials and Design* 29. 526–532.
- K. J. Kim *et al.* (2003). "Formability of AA5182/polypropylene/AA5182 sandwich sheets." *Journal of Materials Processing Technology* 139. 1–7.
- K. Lange *et al.* (1985). "Handbook of Metal Forming." McGraw-Hill. 20.3. 20.18-20.19.
- K. Pohlandt (1989). "Materials testing for the Metal Forming Industry." Springer-Verlag Berlin Heidelberg. p. 107-111.
- Lin Z. Q., Wang W. R. and Chen G. L (2007). "A new strategy to optimize variable blank holder force towards improving the forming limits of aluminum sheet metal forming." *Journal of Materials Processing Technology* 183. 339–346.

- M. A. Ahmetoglu, G. Kinzel and T. Altan (1997). "Forming of aluminum alloys – application of computer simulations and blank holding force control." *Journal of Materials Processing Technology* 71. 147-151.
- M. Firat (2007). "Computer aided analysis and design of sheet metal forming processes: Part I – The finite element modeling concepts." *Materials and Design* 28. 1298–1303.
- M. Kawka *et al.* (2001). "Simulation of wrinkling in sheet metal forming." *Journal of Materials Processing Technology* 109. 283-289.
- M. Samuel (2004). "Numerical and experimental investigations of forming limit diagrams in metal sheets." *Journal of Materials Processing Technology* 153-154. 424–431.
- R. H. Wagoner and J. L. Chenot (2001). "Metal Forming Analysis." Cambridge University Press. 103.
- R. K. Verma and S. Chandra (2006). "An improved model for predicting limiting drawing ratio." *Journal of Materials Processing Technology* 172. 218–224.
- S. A. A. Akbari Mousavi, M. Riahi and A. H. Parast (2007). "Experimental and numerical analyses of explosive free forming." *Journal of Materials Processing Technology* 187–188. 512–516.
- S. Kobayashi *et al.* (1989). "Metal Forming and the Finite Element Method, Oxford University Press." p. 3-4, 90-92 & 93-94.
- T. Yagami, K. Manabe and Y. Yamauchi (2007). "Effect of alternating blank holder motion of drawing and wrinkle elimination on deep-drawability." *Journal of Materials Processing Technology* 187–188. 187–191.

Yoon J.W. and Hong S.H (2006). "Modeling of aluminum alloy sheets based on new anisotropic yield functions." *Journal of Materials Processing Technology* 177.134–137.

Yu Z., Lin Z. and Zhao Y (2007). "Evaluation of fracture limit in automotive aluminum alloy sheet forming." *Materials and Design* 28. 203–207.



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH